
Tummel Bridge GT2 132/11kV Transformer

**Level 1 Condition
Assessment Report
15th July 2020
Report:
TUMBGT2SHET200627
FINAL**

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Executive Summary

Polaris Diagnostics & Engineering Ltd has been commissioned by Scottish Hydro Electric Transmission (SHE Transmission), to carry out a Level 1 condition assessment of Tummel Bridge GT2 132/11kV Transformer.

The level 1 condition assessment has been carried out, based on a review and independent assessment of the historic oil data and SSEN Report T2BP-ACR-0016 Revision 1.0 dated November 2019, both supplied by SHE Transmission.

Based on the assessment of the historical & current asset condition data, GT2 is in reasonably good condition and there is a low likelihood that the transformer condition will deteriorate by ageing during the RIIO T2 period.

The tap changer is recorded as category 4 (serious deterioration or damage that requires specific action in the short term) which specifically relates to the “mechanism”. The inspection data is not explicit as to the nature of the issue, or if this issue has been addressed.

In order to further assess and manage the condition of this transformer, the following recommendations are made:

- Investigate the reported “Category 4” iSIM score for the tap changer. This may require an intervention depending on the findings.
- Continue with routine oil sampling and analysis of the main tank and tap changer.
- In addition to routine oil analysis, the following tests are recommended to assess the rising DDF – These are Interfacial Tension (IFT), Sediment & Sludge & Particle Count.
- Continue with routine maintenance.
- Continue with routine inspection.
- Detailed load flow monitoring.
- 132kV bushings should be oil sampled for DGA and moisture analysis and assessed by the criteria set out in National Grid TGN 82. In addition the bushing power factor and capacitance should be measured. This would require an outage and the removal of the 132kV and 11kV bushings to facilitate the testing.
- Dielectric Frequency Response (DFR) test to assess the condition of the insulation system. This should be considered following assessment of the additional oil analysis to investigate the DDF. This would require an outage and the removal of the 132kV and 11kV bushings to facilitate the testing.



Issue Record

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Issue Date	Issue No	Author	Amendments
27 th June 2020	DRAFT	MJ Gilfeather	-
10 th July 2020	DRAFT v2	MJ Gilfeather	Editorials & Clarifications
15 th July 2020	FINAL	IBB Hunter	Alteration to Report Number

Issue Authority

Author	Issue Authority
Ian B B Hunter Technical Director	Ian B B Hunter Technical Director
	

Review

This document is subject to review.

This document is issued for the party which commissioned it and for specific purposes connected with the above-captioned project only. It should not be relied upon by any other party or used for any other purpose.

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Condition Assessment Level

A level 1 condition assessment was carried out on Tummel Bridge GT2 132/11kV transformer as defined in the table below.

TRANSFORMER CONDITION ASSESSMENT				
LEVEL	DESCRIPTION*	SITE VISIT REQUIRED	OUTAGE REQUIRED	ASSESSMENT CLASS
Level 1	Oil Data and History Provided by Client for Analysis	No	No	Basic
Level 2	Level 1 & Ground Based Visual Survey	Yes	No	Advanced Basic
Level 3	Level 2 & Non-invasive Surveillance (Thermal Survey/RFI Scan of Transformer)	Yes	No	Intermediate
Level 4	Level 3 & Independent Oil Sampling and Analysis in Accordance with IEC 60422	Yes	No	Advanced
Level 5	Level 4 & Overall Visual Survey	Yes	1 day outage	Detailed
Level 6	Level 5 & Electrical Diagnostic Testing (Ranging from Ratio/mag Current, Winding Resistance, Sweep Frequency Response Analysis, Power Factor and Capacitance, Polarisation Index, Bushing Oil Sampling, Bushing Power Factor and Capacitance)	Yes	1-3 days outage	Comprehensive

* Condition assessment can be customised to meet individual client requirements.

Transformer Serial 0404862339

This transformer was manufactured in 1987, and was installed and commissioned at Tummel Bridge 132kV substation.

Tummel Bridge GT2 transformer is installed within an outdoor 132kV air insulated substation (AIS) and is fitted with both 132kV and 11kV oil to air bushings and an on load circuit tap changer. The transformer is furnished with a separate cooler bank which is free breathing.

Electrical Plant Details

Manufacturer:	Bonar Long
Serial Number:	0404862339
Year of Manufacture:	1987
ONAN Rating:	21 MVA
Ratio:	132/11 kV
Vector Group:	Unknown
Impedance:	Unknown
Tap Changer Manufacturer:	ATL
Tap changer Type:	AT319/50/44/300 CF3
Tap Changer Serial Number:	875006
HV Bushings:	Unknown
Oil Type:	Uninhibited, unknown type
Breather Type:	Free Breathing
Moisture Management:	Unknown

Oil Quantities & Weights

Unknown

Transformer Construction

No transformer construction information was made available.

Transformer Defects

Polaris Diagnostics & Engineering Ltd are not aware of any known defects associated with the design of this transformer.

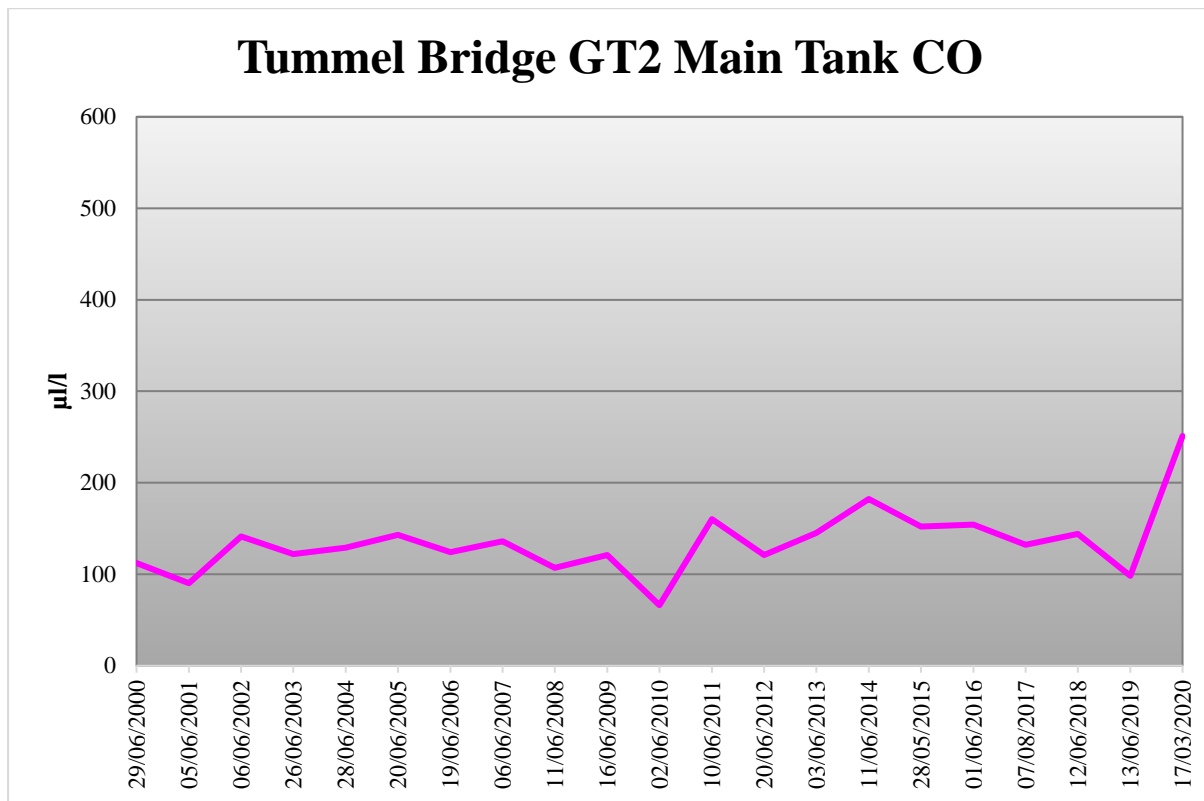
Main Tank Oil History

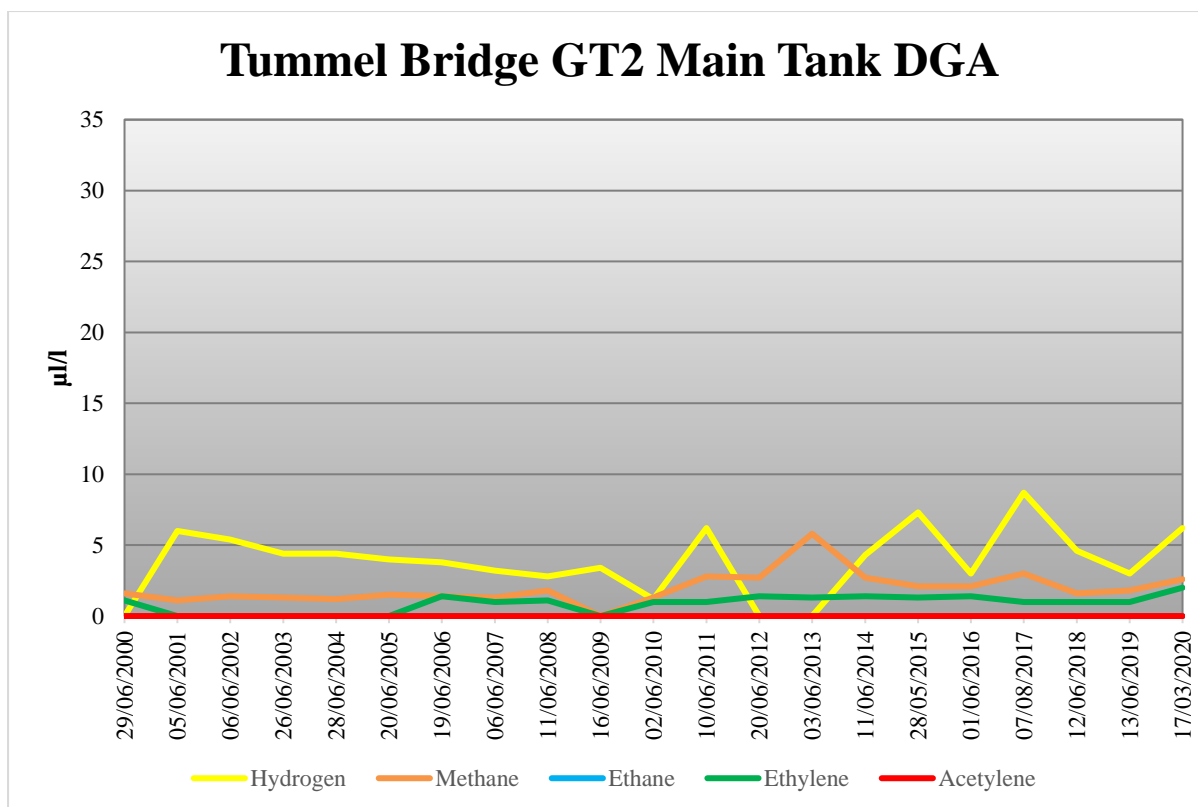
Dissolved Gas Analysis – Main Tank History

Interpretation of the DGA history is carried out using guidance from IEC 60599 “*Mineral Oil Impregnated Electrical Equipment in Service – Guide to the interpretation of dissolved and free gases analysis*”. The available history spans from 2000 to 2020.

As the values of dissolved Carbon Monoxide (CO) are several orders of magnitude greater than all other diagnostic gases, the CO history is plotted separately for clarity.

The CO characteristic is considered relatively stable with only a very minor increasing trend observed over the sample period. All values remain below “typical values” specified in IEC 60599 over the sample period, peaking at 251µl/l in 2020. The paper insulation is likely in good condition.





Hydrogen and thermal gases methane & ethylene are present throughout the DGA history however, all remain at levels well below “typical values” specified in IEC 60599.

Application of the gas ratios, as defined in IEC 60599, [0, 0.5, unspecified] fails to highlight any abnormality through a diagnosis of non-classification. Using the Duval’s triangle method of DGA interpretation, the same gas ratios define a “T2” condition, “Thermal faults, $300^{\circ}\text{C} < T < 700^{\circ}\text{C}$ ”, however, it should be noted that the Duval method being a closed system will always result in a condition being identified. The magnitudes of dissolved gas levels are considered to be too low to accurately diagnose and in this case the DGA would be considered benign.

Analysis of the oil data shows no indication of partial discharge, discharge, or thermal abnormalities being present within the main tank.

Thermal Events:

None

Discharge Events:

None

Dissolved Gas Analysis-Tap Changer

Interpretation of the DGA history is carried out using guidance from IEC 60599 “Mineral Oil Impregnated Electrical Equipment in Service – Guide to the interpretation of dissolved and free gases analysis”.

No tap changer data was made available for analysis.

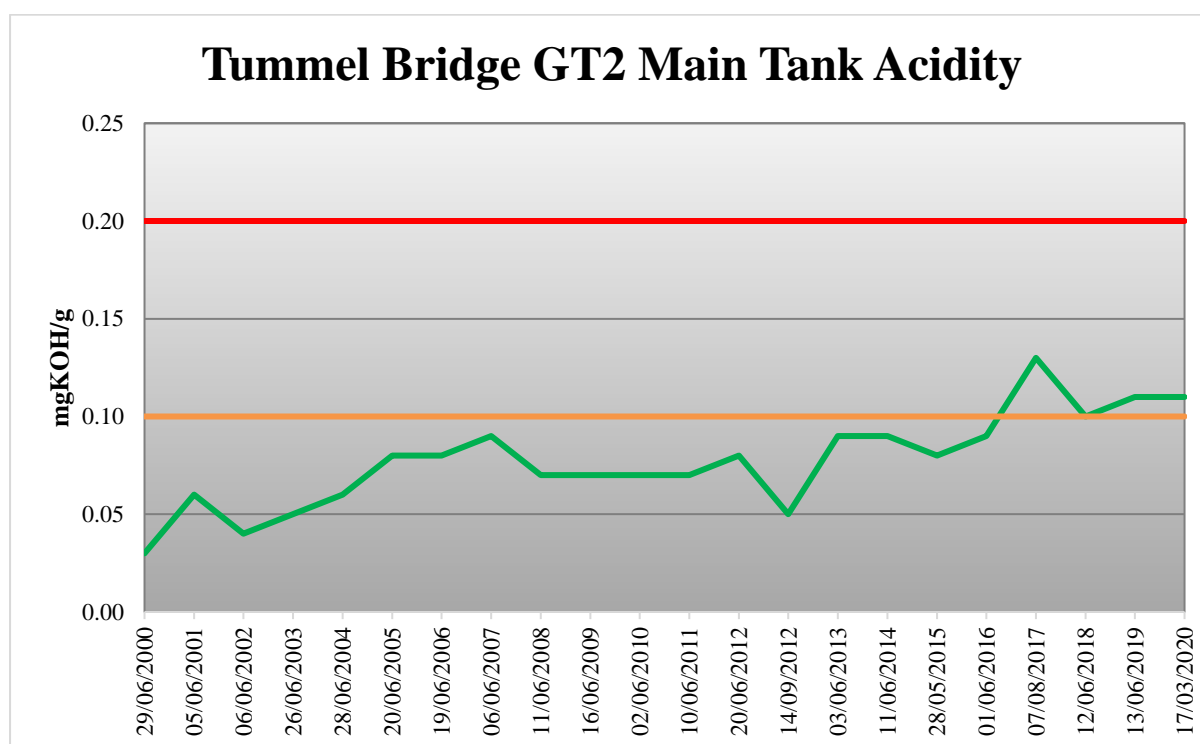
Main Tank Oil Quality Analysis

Interpretation of the oil analysis is carried out in accordance with the requirements of IEC 60422 *“Mineral insulating oils in electrical equipment – supervision and maintenance guidance.”* As this transformer has a primary voltage of 132kV, it falls into the “Category B” limits as defined in the standard.

Acidity

The acidity of used oil is due to the formation of acidic oxidation products. Acids and other oxidation products will in conjunction with water and solid contaminants affect the dielectric and other properties of the oil. Acids have an impact on the degradation of cellulosic materials and maybe responsible for the corrosion of metal parts in a transformer.

IEC 60422 “Category B” Limits for Acidity	
Classification	mgKOH/g
Good	< 0.1
Fair	0.1 – 0.2
Poor	> 0.2

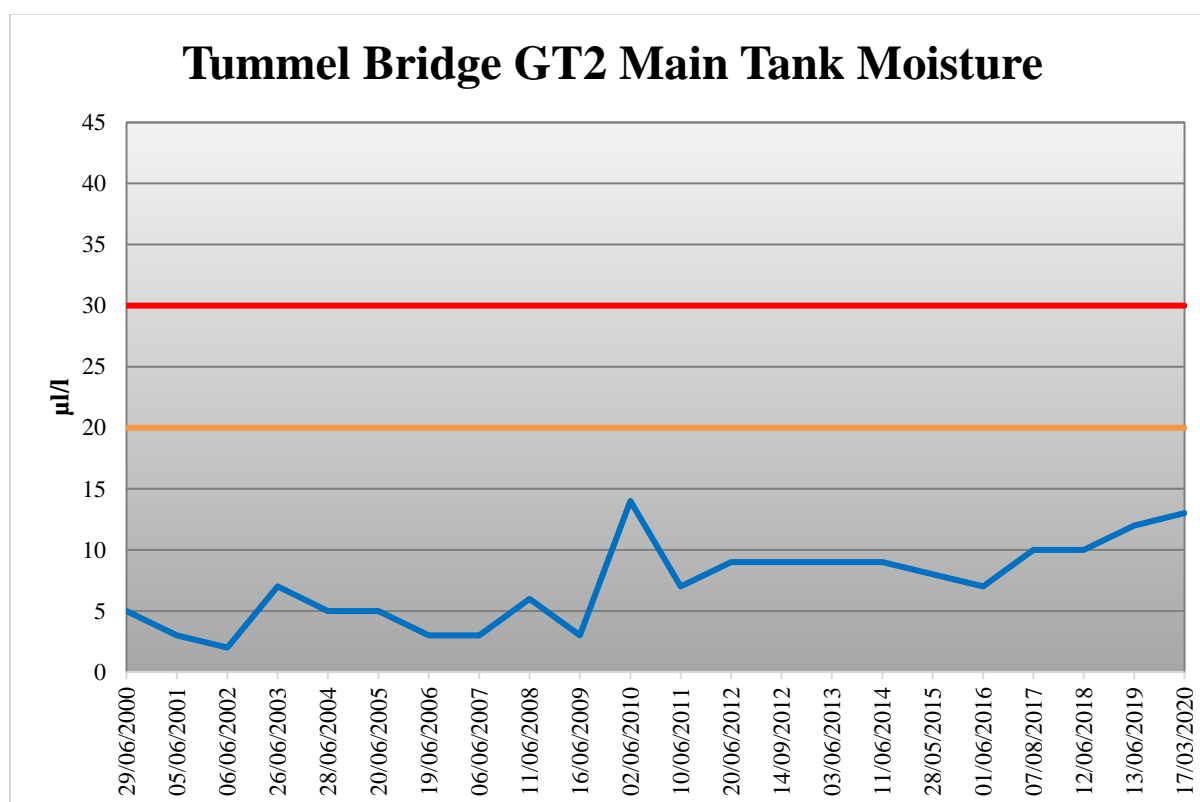


The historical acidity record contains 22 samples taken in the period of 2000 to 2020. The acidity levels are found to exhibit an increasing trend over the sample range indicative of oxidation of the oil. The increasing trend is present from June 2000 to June 2016 however, all samples in this period are categorised as “Good” as defined by IEC 60422 for category B apparatus. The remaining samples in the historical acidity range are all categorised as “Fair”. Overall, the acidity is considered satisfactory but in order to restore the main tank oil to a condition that would defined as “Good” as defined by IEC 60422, the main tank oil would require to be regenerated.

Moisture

The moisture level influences the breakdown voltage of the oil, the solid insulation and affects the ageing characteristics of the liquid and solid insulation. There are two main sources of water, ingress from atmosphere and from the degradation of cellulose in oil.

IEC 60422 “Category B” Limits for Moisture	
Classification	$\mu\text{l/l}$
Good	< 20
Fair	20 -30
Poor	> 30

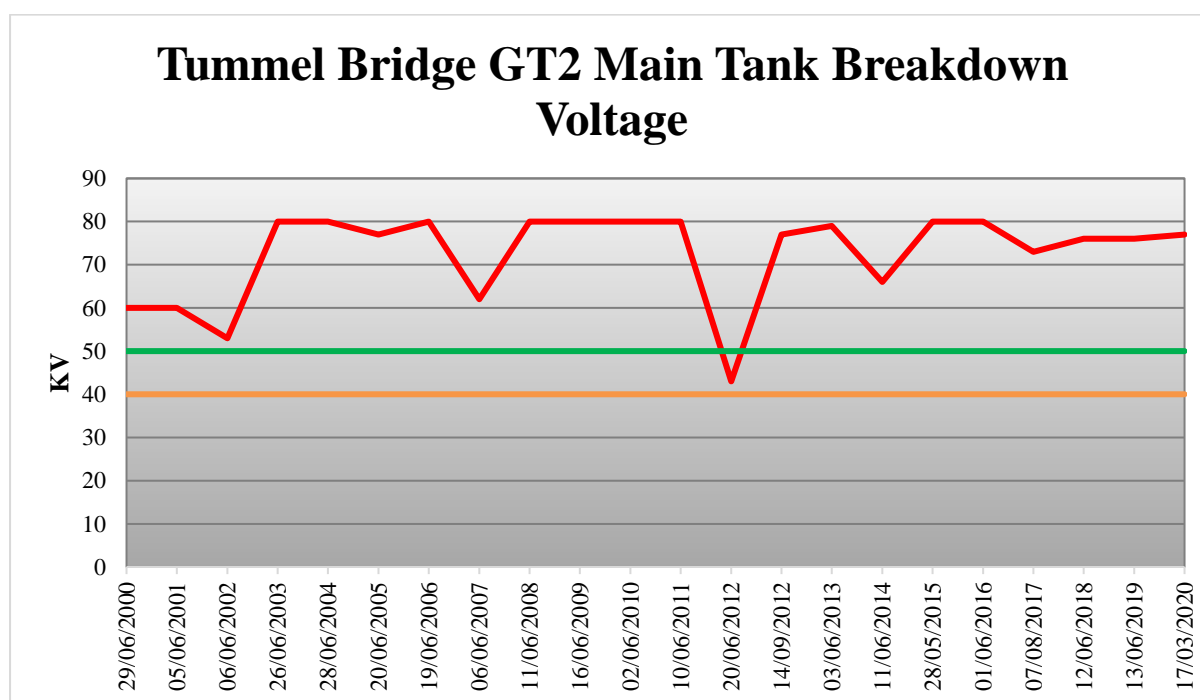


The historical moisture data spans 22 samples taken over the period of 2000 to 2020. Over the operational life of the transformer the moisture levels have been dynamic and, overall, exhibit a minor increasing trend. All historical moisture results are categorised as “Good” as defined by IEC 60422. The peak moisture value is recorded in June 2010 at 14 $\mu\text{l/l}$. The overall moisture trend is satisfactory.

Breakdown Voltage

Breakdown voltage is a measure of the ability of the oil to withstand electric stress. Dry clean oil exhibits an inherently high breakdown voltage. Free water and other polar and non-polar contaminants reduce the breakdown voltage dramatically.

IEC 60422 “Category B” Limits for Breakdown Voltage	
Classification	kV
Good	> 50
Fair	40 - 50
Poor	< 40

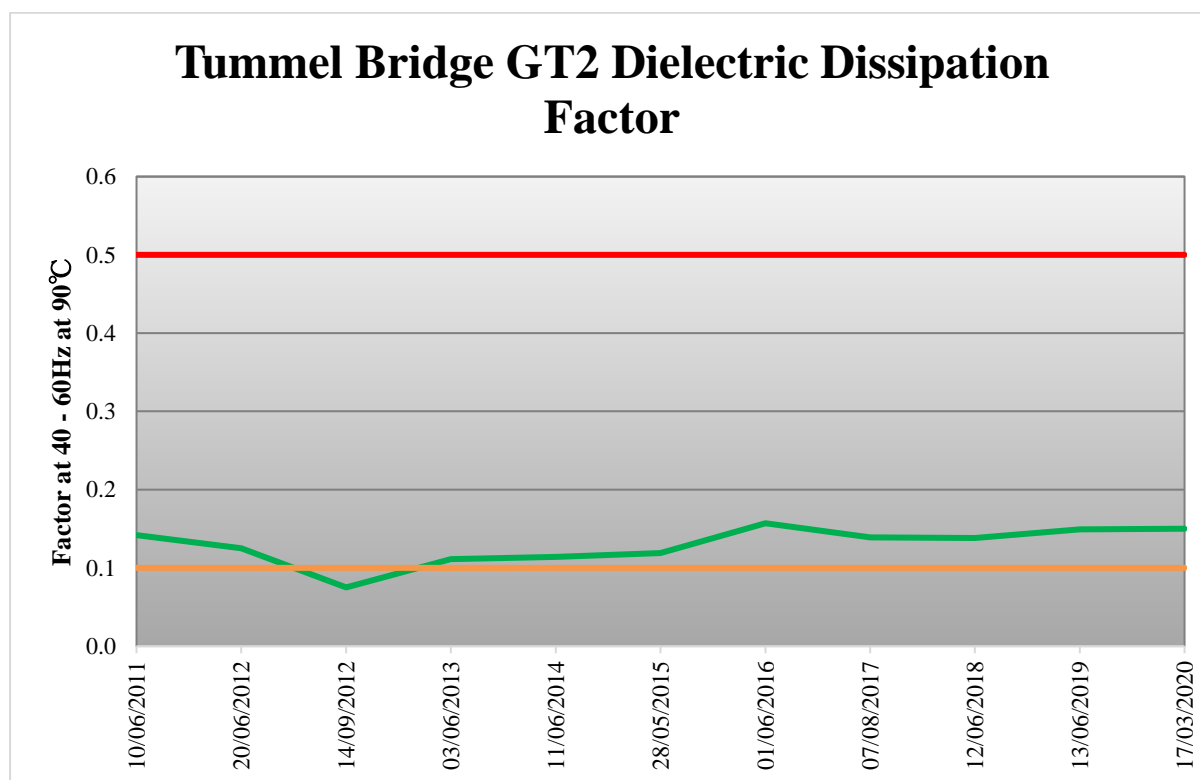


The historical breakdown voltage record spans the period of 2000 to 2020 and is inclusive of 22 samples. Except for the sample from June 2012, which is categorised as “Fair”, all samples are categorised as “Good” as detailed in IEC 60422 for category B apparatus. The overall trend of breakdown voltage levels is dynamic. The reduction in breakdown voltage in June 2012 correlates with a minor increasing moisture level however, other substantial reductions in breakdown voltage do not correlate with an increased moisture level. Overall, the breakdown voltage level trend is satisfactory.

Dielectric Dissipation Factor

The dielectric dissipation factor is sensitive to the presence of soluble polar contaminants and ageing products in the oil. Changes in the levels of contaminants can be monitored by this parameter even when the contamination is so low as to be near the limits of chemical detection.

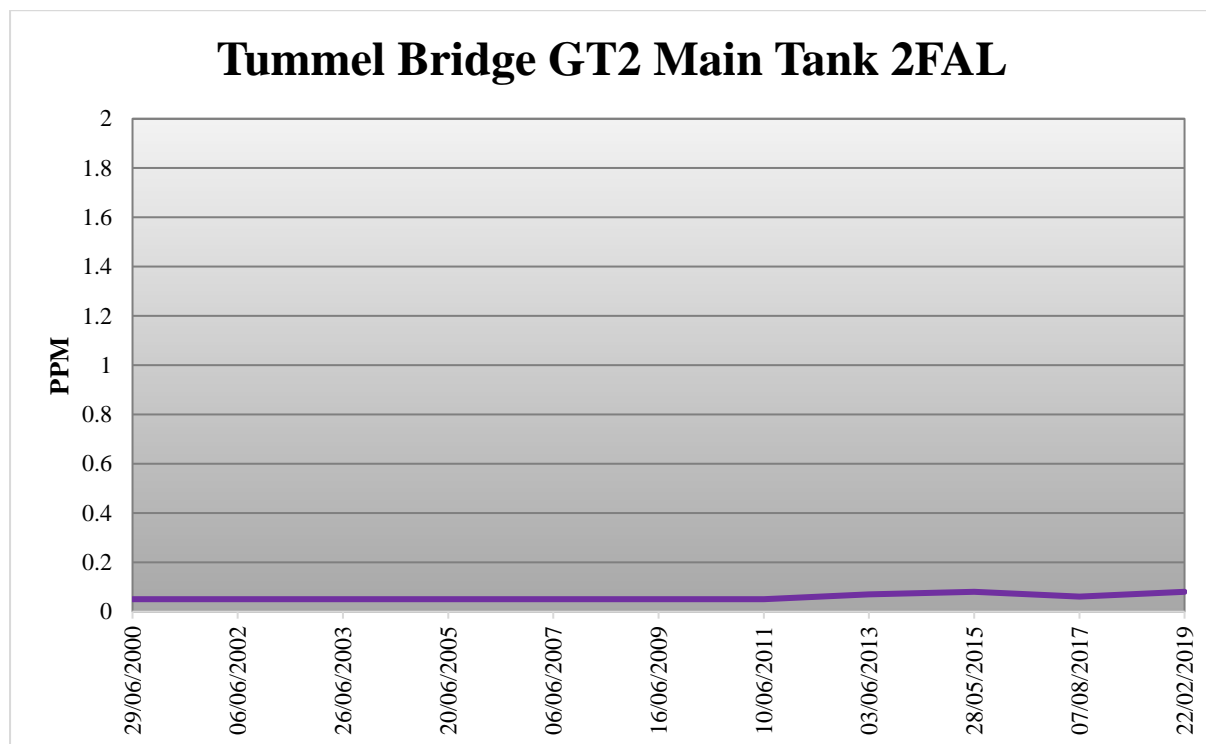
IEC 60422 “Category B” Limits for Dielectric Dissipation Factor	
Classification	kV
Good	< 0.1
Fair	0.1 – 0.5
Poor	> 0.5



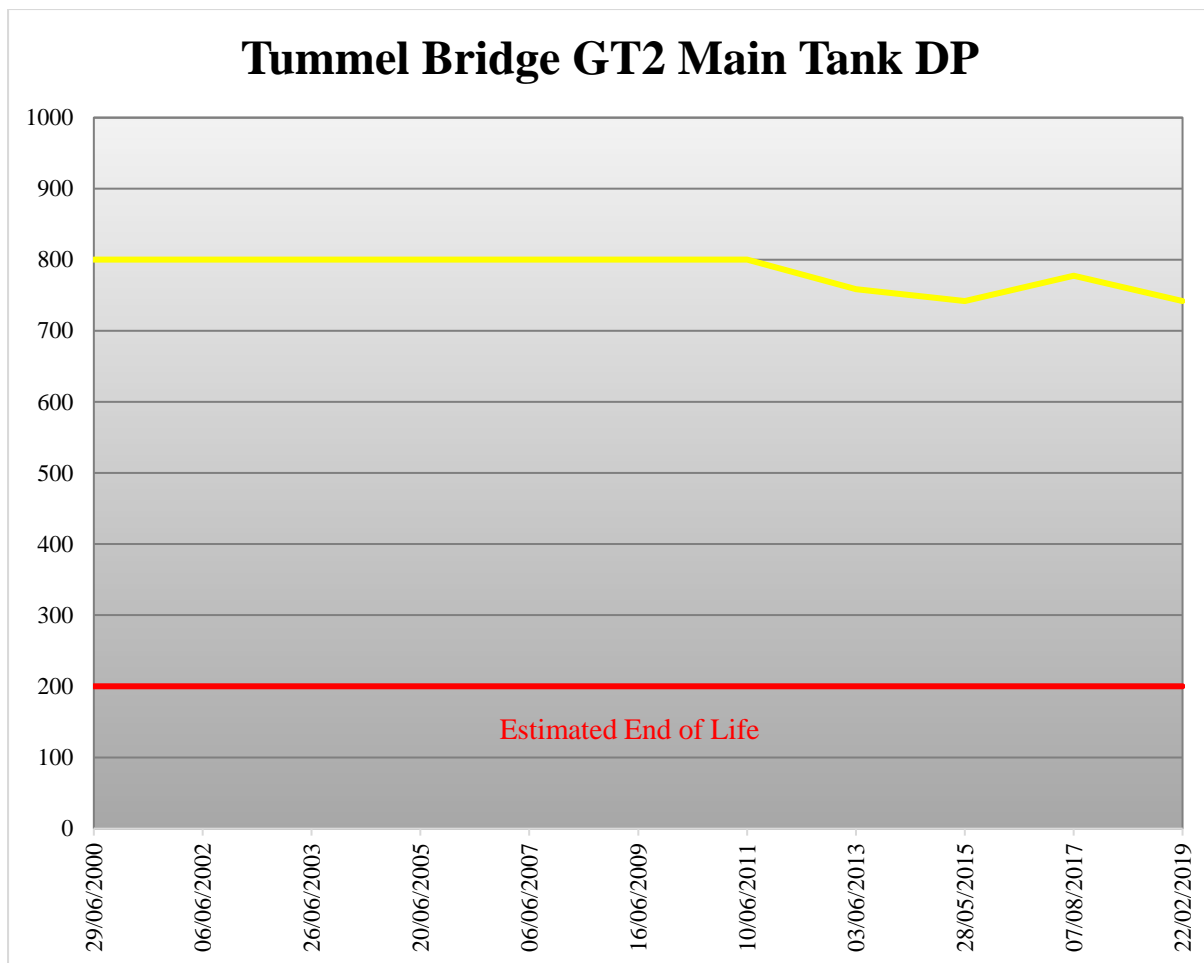
The dielectric dissipation factor spans the period of 2011 to 2020 and includes 11 samples. Over the sample period, the trend exhibited is dynamic yet does indicate a minor increasing trend. Except for the sample from September 2012, which is categorised as “Good”, all samples in the historical range are categorised as “Fair” as defined by IEC 60422 category B apparatus. It may be practical to increase the sampling frequency of GT2 due to the dynamic trend in results. The most recent result for dielectric dissipation factor is “Fair” and is considered representative of the historical sample range.

2FAL

2FAL is a class of furanic compound produced by the degradation and breakdown of cellulose within the transformer. There is a correlation between the measurable 2FAL and the estimated degree of polymerisation (DP), the molecular mechanical strength of the paper within the transformer, although this should be used as an indicator. The 2FAL can be affected by temperature, moisture and acidity, which is not taken into account in the estimation algorithms used. The sampled oil may have been diluted or contaminated during in service operations and is therefore subjected to **high degree of uncertainty**.



The 2FAL record spans from 2000 until the most recent sample, which was taken in February 2019. The 2FAL level remains in a steady state for most of the sample range with the last four samples, from June 2013 to February 2019, exhibiting a very minor increasing trend. The final value recorded, which is also the peak value, is 0.08 (Est DP 742). The link between measured 2FAL and estimated DP is also tenuous and is reliant on an algorithmic relationship, of which there are five different variants. The Chengdong algorithm has been used to relate measured 2FAL to estimated DP. In order to estimate the DP of the insulation system, the highest value of measured 2FAL shall be used (from February 2019). Measured 2FAL of 0.08 gives an estimated DP of 742. The insulation within a new transformer has typically a DP value of 1000. It is generally accepted within the industry that an estimated DP value of 200 is “end of life”. Application of this criteria, results in the transformer having an estimated 67% residual life remaining in the paper insulation. This suggests that the paper insulation is in a good condition.



132kV Bushings

No 132kV bushing data was made available.

General

This section is compiled by making reference to the information contained within SSEN Report T2BP-ACR-0016 Revision 1.0 dated November 2019, henceforth referred to as the document.

Previous Condition Assessments

The iSIM inspection data for GT2 are classified as either category 1 (No visible quantifiable deterioration or damage) or category 2 (Apparent normal wear intervention to be done at the next refurbishment). This highlights that there are no immediate interventions required on GT2.

The tap changer is recorded as category 4 (serious deterioration or damage that requires specific action in the short term) which specifically relates to the “mechanism”. The inspection data is not explicit as to the nature of the issue, or if this issue has been addressed.

Partial Discharge Survey

A partial discharge survey was conducted in November 2014 by Elimpus with no indication of partial discharge being found. There is no evidence of partial discharge activity from transformer GT2 as evidenced by the absence of elevated levels of hydrogen and methane in the dissolved gas analysis.

Infra-Red Thermovision Survey

An infra-red thermovision survey was conducted in May 2016 with two abnormalities being found. The first abnormality was identified as the yellow phase receiver contact of the 132kV disconnector 113, the second abnormality was found on a 33kV post insulator (belonging to SHEPD). In both cases poor connections are identified as the most likely cause of these abnormalities. No thermal abnormalities were found on transformer GT2.

Impulse Protection

Transformer impulse protection is achieved by coordinating gaps fitted to the 132kV bushings.

Load & Duty Cycle

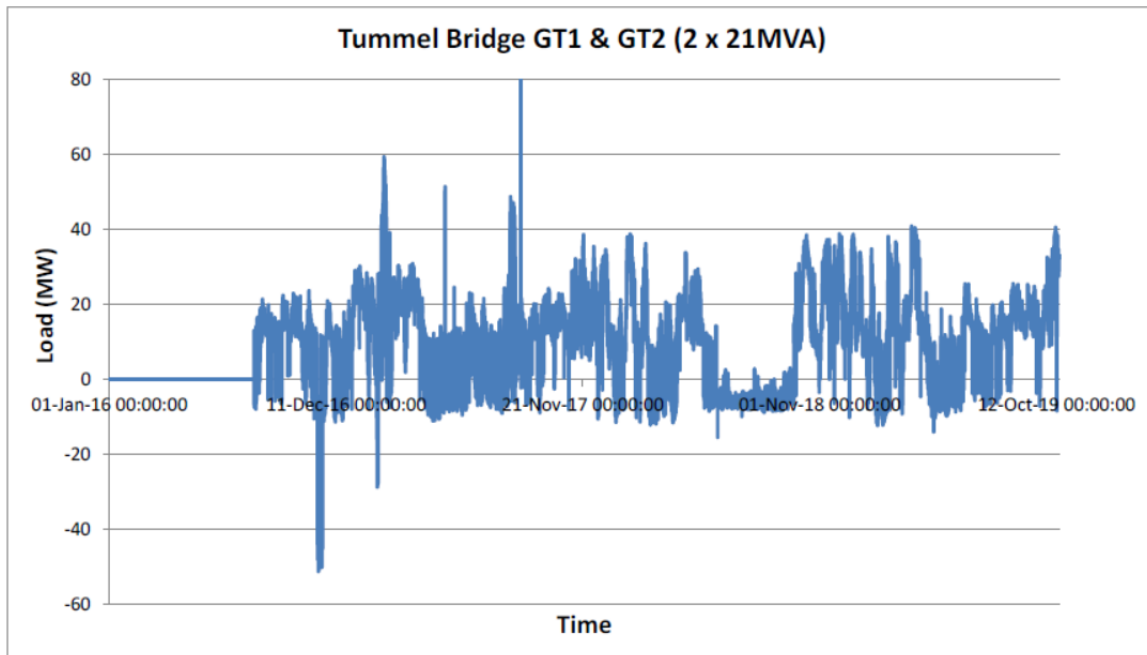


Figure 5.11 from section 5.7 of the document shows a measured combined load flow for GT1 & GT2 for the period of 2016 to 2019. The transformers have a typical maximum combined load flow of around 40MVA, which is within the 42MVA transformer capacity of the substation. There have been three periods of overloading recorded, where the combined transformer capacity has been exceeded. It is not clear from the load flow the exact magnitude or durations of these overloads.

Transformers have an inherent overload capability, which is dependent on the magnitude and duration of the overload. Sustained overload would result in accelerated degradation of the paper winding insulation and would be evidenced in the oil analysis by elevated and increasing levels of CO in the DGA and levels of 2FAL. This is not evident in GT2.

Historical Faults

No historical fault data supplied for GT2.

Maintenance

Maintenance details obtained from PLACAR indicate that routine maintenance has been carried out over the operational lifetime of GT2. The maintenance of GT1 was carried out under contract by SSE Renewables until 2017.

GT2 - MW 132kV Grid Transformer Maintenance - 30/09/2002

GT2TAP - MW 132kV Grid Transformer Tap changer maintenance - 30/09/2002

GT2 - MW 132kV Grid Transformer Maintenance - 16/06/2006

GT2TAP - MW 132kV Grid Transformer Tap changer maintenance - 16/06/2006

GT2 - MW 132kV Grid Transformer Maintenance - 01/09/2010

GT2EAR - MW 132kV Grid Transformer Tap changer maintenance - 01/09/2010

GT2TAP - MW 132kV Grid Transformer Tap changer maintenance - 01/09/2010

GT2TAP - MW 132kV Grid Transformer Tap changer maintenance - 10/09/2012

GT2 - MW 132kV Grid Transformer Maintenance - 10/04/2015

GT2TAP - MW 132kV Grid Transformer Tap changer maintenance - 10/04/2015

GT2 - iSIM Maintenance Record - 21/09/2018

GT2TAP - iSIM Maintenance Record - 21/09/2018

Conclusion

The iSIM inspection data for GT2 are classified as either category 1 (No visible quantifiable deterioration or damage) or category 2 (Apparent normal wear intervention to be done at the next refurbishment). This highlights that there are no immediate interventions required on GT2.

The tap changer is recorded as category 4 (serious deterioration or damage that requires specific action in the short term) which specifically relates to the “mechanism”. The inspection data is not explicit as to the nature of the issue, or if this issue has been addressed.

The DGA does not exhibit any evidence of partial discharge, discharge, or thermal abnormality. The DGA history can be described as benign.

The oil quality parameters comprising of moisture and breakdown voltage are both categorised as “Good” as defined by IEC 60422:2013 indicating that the insulating oil has good dielectric properties. The acidity and DDF are categorised as “Fair” as defined by IEC 60422:2013. In order to restore the acidity to a “Good” category the main tank oil would require to be regenerated. DDF will require further investigation.

Measured 2FAL of 0.08 gives an estimated DP of 742. The insulation within a new transformer has typically a DP value of 1000. It is generally accepted within the industry that an estimated DP value of 200 is “end of life”. Application of this criteria, results in the transformer having an estimated 67% residual life remaining in the paper insulation. This suggests that the paper insulation is in a good condition.

There was no information available on the condition assessment of the 132kV bushings.

The transformers have a typical maximum combined load flow of around 40MVA, which is within the 42MVA transformer capacity of the substation. There have been three periods of overloading recorded, where the combined transformer capacity has been exceeded. It is not clear from the load flow the exact magnitude or durations of these overloads. Transformers have an inherent overload capability, which is dependent on the magnitude and duration of the overload. Sustained overload would result in accelerated degradation of the paper winding insulation and would be evidenced in the oil analysis by coincident elevated and increasing levels of CO in the DGA and levels of 2FAL. This is not evident in GT2.

This transformer is presently in reasonable condition.

Recommendations

In order to further assess and manage the condition of this transformer, the following recommendations are made:

- Investigate the reported “Category 4” iSIM score for the tap changer. This may require an intervention depending on the findings.
- Continue with routine oil sampling and analysis of the main tank and tap changer.
- In addition to routine oil analysis, the following tests are recommended to assess the rising DDF – These are Interfacial Tension (IFT), Sediment & Sludge & Particle Count.
- Continue with routine maintenance.
- Continue with routine inspection.
- Detailed load flow monitoring.
- 132kV bushings should be oil sampled for DGA and moisture analysis and assessed by the criteria set out in National Grid TGN 82. In addition the bushing power factor and capacitance should be measured. This would require an outage and the removal of the 132kV and 11kV bushings to facilitate the testing.
- Dielectric Frequency Response (DFR) test to assess the condition of the insulation system. This should be considered following assessment of the additional oil analysis to investigate the DDF. This would require an outage and the removal of the 132kV and 11kV bushings to facilitate the testing.